



February 24, 2020

Lavington Pellet Limited Partnership
9900 School Road
Coldstream, B.C.,
V1B 3C7

Attention: **Jamie Colliss**
Re: **Air Emission Testing of February 11, 2020**
 Permit 107369, ME1718-562

As requested our firm provided a series of air emission tests at your facility in Lavington BC.

Testing Parameters

- CF-12
 - o Total Particulate Testing (including Condensable Organics) State of Oregon Method 7

Key Personnel

- Report Generation: Matt McCall 250-542-5118
- Field Supervisor: Dan Lawrence 250-542-5118
- Plant Contact: Jamie Colliss 250-542-1720

All testing procedures were conducted in accordance with acceptable methodologies as listed in the latest revision of the BC Field Sampling Manual. A copy of the method and/or Sampling Manual are digitally available upon request. All lab analysis for back half condensable organic fractions was analyzed by EXOVA Laboratories in Surrey BC. A copy of their report can be found in the Appendix of this report.

Results are summarized immediately following this cover letter. Please note that all results are expressed on a dry basis and reference conditions of 20 deg C, 1 atm pressure.

If you have any questions or concerns please don't hesitate to contact us at your earliest convenience.

Sincerely,

MCCALL ENVIRONMENTAL

Matt McCall

Summary of Test Results

CF12 February 11, 2020 Summary of Test Results 1-3

Particulate Results

Parameter	Test 1	Test 2	Test 3	Average	Permit
Start Time	9:00	10:15	11:30	N/A	
Stop Time	10:04	11:19	12:35	N/A	
Gas Temperature (°C)	26.3	33.4	34.5	31.4	
% Moisture	1.2	1.3	1.4	1.3	
Velocity (m/sec)	19.00	19.27	19.34	19.20	
ACFM	73429	74448	74742	74206	
Std. Dry Flow Rate (m ³ /sec)	31.27	30.93	30.90	31.04	34.00
Oxygen in % (dry basis)	21.00	21.00	21.00	21.00	
Carbon Dioxide % (dry basis)	0.00	0.00	0.00	0.00	
Tot Part. Dry Basis ref. Cond. (mg/m ³)	3.55	4.91	2.89	3.78	10.00
Front Half Filterable Particulate (mg/m ³)	1.58	2.91	0.90	1.79	
Back Half Cond. Organics (mg/m ³)	1.97	2.00	1.99	1.99	
Mass Emission Rate (kg/hr)	0.01	0.01	0.01	0.01	



**Pinnacle Pellet
CF-12 Baghouse Stack
Lavington BC**

Feb 11/20

Permit Number: 107369

AVERAGE OF AIR EMISSION TESTS 1 TO 3

Gas Temperature:	89 °F	31 °C
Moisture Content (by volume):	1.31 %	
Average Stack Gas Velocity:	63.0 ft/sec	19.20 m/sec
Total Actual Gas Flow Rate:	74206 ACFM	
Dry Gas flow Rate at Reference Conditions:	65763 SCFM	31.04 m ³ /sec
Total Particulate Concentration:		
Dry Basis Actual at Reference Conditions	0.002 gr/ft ³	3.8 mg/m ³
Front Half Particulate	0.001 gr/ft ³	1.8 mg/m ³
Back Half Condensibles	0.001 gr/ft ³	2.0 mg/m ³
Mass Emission Rate	0.02 lbs/hr	0.01 kg/hr

SUMMARY OF AIR EMISSION TESTS

TEST 1:

Gas Temperature:	79 °F	26 °C
Moisture Content (by volume):	1.2 %	
Average Stack Gas Velocity:	62.3 ft/sec	19.0 m/sec
Total Actual Gas Flow Rate:	73429 ACFM	
Dry Gas flow Rate at Reference Conditions:	66267 SCFM	31.3 m ³ /sec
Total Particulate Concentration:		
Dry Basis Actual at Reference Conditions	.002 gr/ft ³	3.5 mg/m ³
Front Half Particulate	.001 gr/ft ³	1.6 mg/m ³
Back Half Condensibles	.001 gr/ft ³	2.0 mg/m ³
Mass Emission Rate	0.01 lbs/hr	0.01 kg/hr

TEST 2:

Gas Temperature:	92 °F	33 °C
Moisture Content (by volume):	1.3 %	
Average Stack Gas Velocity:	63.2 ft/sec	19.3 m/sec
Total Actual Gas Flow Rate:	74448 ACFM	
Dry Gas flow Rate at Reference Conditions:	65546 SCFM	30.9 m ³ /sec
Total Particulate Concentration:		
Dry Basis Actual at Reference Conditions	.002 gr/ft ³	4.9 mg/m ³
Front Half Particulate	.001 gr/ft ³	2.9 mg/m ³
Back Half Condensibles	.001 gr/ft ³	2.0 mg/m ³
Mass Emission Rate	0.02 lbs/hr	0.01 kg/hr

TEST 3:

Gas Temperature:	94 °F	35 °C
Moisture Content (by volume):	1.4 %	
Average Stack Gas Velocity:	63.5 ft/sec	19.3 m/sec
Total Actual Gas Flow Rate:	74742 ACFM	
Dry Gas flow Rate at Reference Conditions:	65475 SCFM	30.9 m ³ /sec
Total Particulate Concentration:		
Dry Basis Actual at Reference Conditions	.001 gr/ft ³	2.9 mg/m ³
Front Half Particulate	.000 gr/ft ³	.9 mg/m ³
Back Half Condensibles	.001 gr/ft ³	2.0 mg/m ³
Mass Emission Rate	0.01 lbs/hr	0.01 kg/hr

DATA FOR TESTS 1 TO 3

Client: Pinnacle Pellet
Plant Location: Lavington BC
Process: CF-12 Baghouse Stack
Permit Number: 107369
Job Number: ME1718-562
Pollution Control Permit: 10.0 mg/m3 34 m3/sec
Number of Tests: 3 tests
Minutes per Point: 2.5 minutes

	TEST 1	TEST 2	TEST 3
Filter Number:	29	30	31
Date of Test:	Feb 11/20	Feb 11/20	Feb 11/20
Start Time:	9:00	10:15	11:30
Stop Time:	10:04	11:19	12:35
On-line Sampling Time:	60	60	60
Testing Personnel:	DL/KS	DL/KS	DL/KS
Sampler Model:	1013	1013	1013
Barometric Pressure("Hg):	27.95	27.95	27.95
Static Pressure("H₂O):	-0.55	-0.55	-0.55
%CO₂:	0.0	0.0	0.0
%O₂:	21.0	21.0	21.0
%CO:	0.0	0.0	0.0
%N₂:	79.0	79.0	79.0
Diameter of Nozzle(inches):	0.180	0.180	0.180
Meter Factor:	1.0033	1.0033	1.0033
Type-S Pitot Tube Coefficient:	0.84158	0.84158	0.84158
Cross Sectional Area of Stack(ft²):	19.63	19.63	19.63
Impinger Condensate(g):	2	2	2
Weight of Moisture in Silica Gel(g):	7.0	8.0	9.0
Weight of Filter Particulate(g):	0.0005	0.0005	0.0003
Weight of Probe Washings(g):	0.0011	0.0024	0.0006
Weight of Impinger Content Organic(g):	0.0020	0.0020	0.0020
Total Weight of Particulate(g):	0.0036	0.0049	0.0029



**Pinnacle Pellet
CF-12 Baghouse Stack
Pinnacle Pellet**

Data for TEST 1

OVERALL ISOKINETICS - TEST 1: 1.002

Delta P:	1.116 "H₂O	Us avg:	62.34 ft/sec
Delta H:	1.408	ACFM:	73429 ft³/min
Tm avg:	514.8 °R	SDCFM:	66267 ft³/min
Ts avg:	539.4 °R	Vm std:	35.84 ft³
Bwo:	0.012	Vm corr:	37.27 ft³
Md:	28.84	Vm:	37.15 ft³
Ms:	28.71	MF:	1.0033
Pb:	27.95 "Hg	PCON:	3.55 mg/m³
Pm:	28.05 "Hg	ERAT:	0.40 kg/hr
Ps:	27.91 "Hg		

Data for TEST 2

OVERALL ISOKINETICS - TEST 2: 0.996

Delta P:	1.120 "H₂O	Us avg:	63.21 ft/sec
Delta H:	1.452	ACFM:	74448 ft³/min
Tm avg:	539.8 °R	SDCFM:	65546 ft³/min
Ts avg:	552.0 °R	Vm std:	35.24 ft³
Bwo:	0.013	Vm corr:	38.42 ft³
Md:	28.84	Vm:	38.29 ft³
Ms:	28.70	MF:	1.0033
Pb:	27.95 "Hg	PCON:	4.91 mg/m³
Pm:	28.06 "Hg	ERAT:	0.55 kg/hr
Ps:	27.91 "Hg		

Data for TEST 3

OVERALL ISOKINETICS - TEST 3: 1.002

Delta P:	1.124 "H₂O	Us avg:	63.46 ft/sec
Delta H:	1.457	ACFM:	74742 ft³/min
Tm avg:	541.4 °R	SDCFM:	65475 ft³/min
Ts avg:	554.1 °R	Vm std:	35.42 ft³
Bwo:	0.014	Vm corr:	38.73 ft³
Md:	28.84	Vm:	38.60 ft³
Ms:	28.68	MF:	1.0033
Pb:	27.95 "Hg	PCON:	2.89 mg/m³
Pm:	28.06 "Hg	ERAT:	0.32 kg/hr
Ps:	27.91 "Hg		

Air Emission Monitoring Procedure

Particulate Sampling (Napp-Baldwin Model 31 Sampler)

Particulate sampling and gas velocity measurements were conducted using a Napp-Baldwin Model 31 stack sampler in accordance with the methods specified in EPA Method 5 (See Figure 1).

The air discharge was sampled isokinetically at the centroid of a series of equal area segments across the duct or stack. The stack gas velocity and temperature were recorded during the sample collection period with a calibrated pitot tube and thermocouple mounted on the sampling probe. The sample was delivered from the probe to a cyclone and a filter holder containing a 110mm Type A glass fiber filter. The gas sample was then drawn in through a series of four glass impingers which condensed and absorbed the water from the gas. A leakless vacuum pump carried the sampled gas through a dry gas test meter where the volume, temperature, and pressure were measured; and finally through a flow indicating orifice which allowed for the rapid adjustment to isokinetic sampling rates.

At the end of each test, the probe interior, cyclone and connecting tubing from the probe to the filter housing were rinsed with distilled water and acetone. These washings were evaporated to dryness and the resulting solids were weighed. The weight of the cyclone flask and the filter was used together with the weight of solids in the washings to calculate the particulate concentration. The moisture content of the stack gas was determined from the quantity of water condensed in the impingers and absorbed in the silica gel.

O₂, CO₂, CO (where applicable)

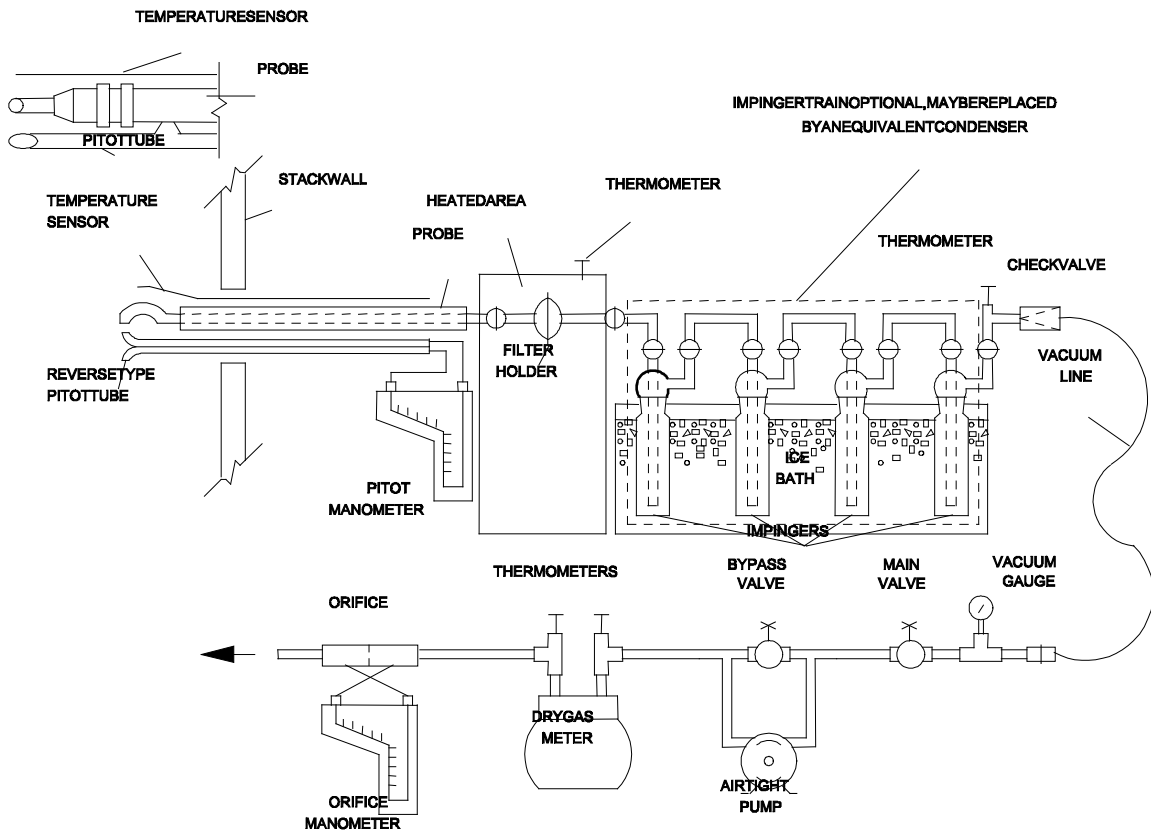
O₂, CO₂, and CO were found using either Fuji Analytical Analyzer by means of infrared and paramagnetic technology (EPA 3A) or by fyrite (EPA Method 3).

NO_x (where applicable)

NO_x was found using and API Model 252 NO_x analyzer that utilizes chemiluminescent technology. Stack gas was Samples were taken over a minimum period of three hours.

VOC's (where applicable)

Hydrocarbons were measured in accordance with EPA method 25A. Samples were drawn in one hour test runs using a total hydrocarbon analyzer that utilizes Flame Ionization Technology.



EPA Method 5 Diagram- Figure 1

CALCULATIONS

Carry out calculations, retaining at least one extra decimal figure beyond that of the acquired data. Round off figures after the final calculation. Other forms of the equations may be used as long as they give equivalent results.

Nomenclature.

- A_n = Cross-sectional area of nozzle, m^2 (ft^2).
 B_{ws} = Water vapor in the gas stream, proportion by volume.
 C_a = Acetone blank residue concentration, mg/g .
 c_s = Concentration of particulate matter in stack gas, dry basis, corrected to standard conditions, $g/dscm$ ($g/dscf$).
 I = Percent of isokinetic sampling.
 L_a = Maximum acceptable leakage rate for either a pretest leak check or for a leak check following a component change; equal to $0.00057 m^3/min$ ($0.02 cfm$) or 4 percent of the average sampling rate, whichever is less.
 L_i = Individual leakage rate observed during the leak check conducted prior to the " i^{th} " component change ($i = 1, 2, 3...n$), m^3/min (cfm).
 L_p = Leakage rate observed during the post-test leak check, m^3/min (cfm).
 m_a = Mass of residue of acetone after evaporation, mg .
 m_n = Total amount of particulate matter collected, mg .
 M_w = Molecular weight of water, $18.0 g/g\text{-mole}$ ($18.0 lb/lb\text{-mole}$).
 P_{bar} = Barometric pressure at the sampling site, $mm Hg$ ($in. Hg$).
 P_s = Absolute stack gas pressure, $mm Hg$ ($in. Hg$).
 P_{std} = Standard absolute pressure, $760 mm Hg$ ($29.92 in. Hg$).
 R = Ideal gas constant, $0.06236 \frac{[(mmHg)(m^3)]}{[(^{\circ}K)(g\text{-mole})]}$
 $\{21.85 \frac{[(in. Hg)(ft^3)]}{[(^{\circ}R)(lb\text{-mole})]}\}$.
 T_m = Absolute average DGM temperature (see Figure 5-2), $^{\circ}K$ ($^{\circ}R$).
 T_s = Absolute average stack gas temperature (see Figure 5-2), $^{\circ}K$ ($^{\circ}R$).
 T_{std} = Standard absolute temperature, $293^{\circ}K$ ($528^{\circ}R$).
 V_a = Volume of acetone blank, ml .
 V_{aw} = Volume of acetone used in wash, ml .
 V_{lc} = Total volume liquid collected in impingers and silica gel (see Figure 5-3), ml .
 V_m = Volume of gas sample as measured by dry gas meter, dcm (dcf).
 $V_{m(std)}$ = Volume of gas sample measured by the dry gas meter, corrected to standard conditions, $dscm$ ($dscf$).
 $V_{w(std)}$ = Volume of water vapor in the gas sample, corrected to standard conditions, scm (scf).
 v_s = Stack gas velocity, calculated by Method 2, Equation 2-9, using data obtained from Method 5, m/sec (ft/sec).
 W_a = Weight of residue in acetone wash, mg .
 Y = Dry gas meter calibration factor.
 ΔH = Average pressure differential across the orifice meter (see Figure 5-2), $mm H_2O$ ($in. H_2O$).
 ρ_a = Density of acetone, mg/ml (see label on bottle).
 ρ_w = Density of water, $0.9982 g/ml$ ($0.002201 lb/ml$).
 θ = Total sampling time, min .
 θ_1 = Sampling time interval, from the beginning of a run until the first component change, min .
 θ_i = Sampling time interval, between two successive component changes, beginning with the interval between the first and second changes, min .
 θ_p = Sampling time interval, from the final (n^{th}) component change until the end of the sampling run, min .
 13.6 = Specific gravity of mercury.
 60 = Sec/min .
 100 = Conversion to percent.

Average Dry Gas Meter Temperature and Average Orifice Pressure Drop.

Dry Gas Volume. Correct the sample volume measured by the dry gas meter to standard conditions (20°C, 760 mm Hg or 68°F, 29.92 in. Hg) by using Equation 5-1.

$$V_{m(\text{std})} = V_m Y \left(\frac{T_{\text{std}}}{T_m} \right) \left[\frac{P_{\text{bar}} + \frac{\Delta H}{13.6}}{P_{\text{std}}} \right]$$

$$= K_1 V_m Y \frac{P_{\text{bar}} + \left(\frac{\Delta H}{13.6} \right)}{T_m}$$
Eq. 5-1

where:

$$K_1 = 0.3858 \text{ } ^\circ\text{K/mm Hg for metric units,}$$

$$= 17.64 \text{ } ^\circ\text{R/in. Hg for English units.}$$

NOTE: Equation 5-1 can be used as written unless leakage rate observed during any of the mandatory leak checks (i.e., the post-test leak check or leak checks conducted prior to component changes) exceeds L_a . If L_p or L_i exceeds L_a , Equation 5-1 must be modified as follows:

(a) Case I. No component changes made during sampling run. In this case, replace V_m in Equation 5-1 with the expression:

$$[V_m - (L_p - L_a) \theta]$$

(b) Case II. One or more component changes made during the sampling run. In this case, replace V_m in Equation 5-1 by the expression:

$$\left[V_m - (L_1 - L_a) \theta_1 - \sum_{i=2}^n (L_i - L_a) \theta_i - (L_p - L_a) \theta_p \right]$$

and substitute only for those leakage rates (L_i or L_p) which exceed L_a .

Volume of Water Vapor.

$$V_{w(\text{std})} = \frac{V_{lc} \rho_w R T_{\text{std}}}{M_w P_{\text{std}}} = K_2 V_{lc}$$
Eq. 5-2

where:

$$K_2 = 0.001333 \text{ m}^3/\text{ml for metric units,}$$

$$= 0.04707 \text{ ft}^3/\text{ml for English units.}$$

Moisture Content.

$$B_{ws} = \frac{V_{w(\text{std})}}{V_{m(\text{std})} + V_{w(\text{std})}} \quad \text{Eq. 5-3}$$

Acetone Blank Concentration.

$$C_a = \frac{m_a}{V_a \rho_a} \quad \text{Eq. 5-4}$$

Acetone Wash Blank.

$$W_a = C_a V_{aw} \rho_a \quad \text{Eq. 5-5}$$

Total Particulate Weight. Determine the total particulate matter catch from the sum of the weights obtained from Containers 1 and 2 less the acetone blank (see Figure 5-3).

Particulate Concentration.

$$C_s = (0.001 \text{ g/mg})(m_n / V_{m(\text{std})}) \quad \text{Eq. 5-6}$$

Conversion Factors:

<u>From</u>	<u>To</u>	<u>Multiply by</u>
scf	m ³	0.02832
g/ft ³	gr/ft ³	15.43
g/ft ³	lb/ft ³	2.205 x 10 ⁻³
g/ft ³	g/m ³	35.31

Isokinetic Variation.**Calculation from Raw Data.**

$$I = \frac{100 T_s [K_3 V_{1c} + (V_m Y / T_m)(P_{\text{bar}} + \Delta H / 13.6)]}{60 \theta v_s P_s A_n} \quad \text{Eq. 5-7}$$

where:

$K_3 = 0.003454 [(\text{mm Hg})(\text{m}^3)]/[(\text{ml})(^\circ\text{K})]$ for metric units,

$= 0.002669 [(\text{in. Hg})(\text{ft}^3)]/[(\text{ml})(^\circ\text{R})]$ for English units.

Calculation from Intermediate Values.

$$I = \frac{100 T_s V_{m(\text{std})} P_{\text{std}}}{60 T_{\text{std}} v_s \theta A_n P_s (1 - B_{\text{ws}})} \quad \text{Eq. 5-8}$$

$$= \frac{K_4 T_s V_{m(\text{std})}}{P_s v_s A_n \theta (1 - B_{\text{ws}})}$$

where:

$K_4 = 4.320$ for metric units,

$= 0.09450$ for English units.

Acceptable Results. If 90 percent $\leq I \leq 110$ percent, the results are acceptable. If the PM results are low in comparison to the standard, and "I" is over 110 percent or less than 90 percent, the Administrator may opt to accept the results. Citation 4 in the Bibliography may be used to make acceptability judgments. If "I" is judged to unacceptable, reject the results, and repeat the test.

Average Stack Gas Velocity.

$$v_s = K_p C_p (\sqrt{\Delta p})_{\text{avg}} \sqrt{\frac{T_{s(\text{avg})}}{P_s M_s}}$$

Average Stack Gas Dry Volumetric Flow Rate.

$$Q_{\text{sd}} = 3,600(1 - B_{\text{ws}}) v_s A \frac{T_{\text{std}}}{T_{s(\text{avg})}} \frac{P_s}{P_{\text{std}}}$$

where:

- A = Cross-sectional area of stack, m^2 (ft^2).
- B_{ws} = Water vapor in the gas stream (from Method 5 or Reference Method 4), proportion by volume.
- C_p = Pitot tube coefficient, dimensionless.
- K_p = Pitot tube constant,
- M_d = Molecular weight of stack gas, dry basis (see Section 3.6), g/gmole (lb/lb-mole).
- M_s = Molecular weight of stack gas, wet basis, g/g-mole (lb/lb-mole).

$$= M_d (1 - B_{\text{ws}}) + 18.0 B_{\text{ws}} \quad \text{Eq. 2-5}$$

- P_{bar} = Barometric pressure at measurement site, mm Hg (in. Hg).
- P_g = Stack static pressure, mm Hg (in. Hg).
- P_s = Absolute stack pressure, mm Hg (in. Hg),

$$= P_{\text{bar}} + P_g$$

- P_{std} = Standard absolute pressure, 760 mm Hg (29.92 in. Hg).
- Q_{sd} = Dry volumetric stack gas flow rate corrected to standard conditions, dsm^3/hr (dscf/hr).
- t_s = Stack temperature, $^{\circ}\text{C}$ ($^{\circ}\text{F}$).
- T_s = Absolute stack temperature, $^{\circ}\text{K}$ ($^{\circ}\text{R}$).

Calibration Certificate for S-Type Pitot Tube

Date: 5-Jan-20 *Barometric Pressure ("Hg):* 28.25
Pitot I.D.: **242** *Wind Tunnel Temperature (° F):* 71.0
Nozzle: 0.250

<i>Wind Velocity (ft/sec)</i>	<i>Ref.Pitot ("H₂O)</i>	<i>S-Type Pitot ("H₂O)</i>	<i>Pitot Factor</i>
13.07	0.03676	0.05091	0.84120
19.56	0.08230	0.11495	0.83765
42.21	0.38343	0.53104	0.84123
64.61	0.89820	1.20776	0.85375
84.98	1.55395	2.11982	0.84763
106.66	2.44808	3.49980	0.82799

Average= 0.84158

Note: The new pitot tip should be installed so that the serial number engraved is aligned directly into the gas stream.

**CALIBRATION CERTIFICATE
DRY GAS METER**

DATE: 09-Jan-20

CONSOLE MANUF.: NAPP/MILLENNIUM MODEL 32

CONSOLE I.D.: MU 1012

PARAMETER SUMMARY	RUN #1	RUN #2	RUN #3
Ta = Ambient (WTM) Temperature (oF.)	56.0	56.0	56.0
P=Pres. Differential at WTM ("Hg)	0.0773	0.1472	0.2208
Pb= Atmospheric Pressure ("Hg)	28.25	28.25	28.25
Pv= Vapour Pressure Water at Temp. Ta ("Hg)	0.4517	0.4517	0.4517
H=Pres. Differential at Orifice	1.0	2.0	3.0
Ti= Dry Test Meter Inlet Temp. (oF.)	71.0	68.0	75.0
To= Dry Test Meter Outlet Temp. (oF.)	69.0	65.0	73.0
Ri= Initial Dry Test volume (ft3)	0.00	0.00	0.00
Rf= Final Dry Test Volume (ft3)	5.03	4.96	5.00
Vi= Initial Wet Test Volume (ft3)	0.0	0.0	0.0
Vf= Final Wet Test Volume (ft3)	5.000	5.000	5.000
Pw= $P_b - (^P/13.59)$ "Hg	28.1727	28.1028	28.0292
Pd= $P_b + (^H/13.59)$ "Hg	28.3236	28.3972	28.4708
Tw= Ta +460 (oR.)	516.0	516.0	516.0
Td= $[(T_i + T_o)/2] + 460$ (oR.)	530.0	526.5	534.0
Bw= Pv/Pb ("Hg)	0.0160	0.0160	0.0160
WET TEST METER FACTOR (WTMF)	0.9922	0.9922	0.9922
ated Y Value)(WTMF)	0.9915	0.9938	0.9947
Y (MEAN)(WTMF) =	0.9934		

N.R. MCCALL & ASSOCIATES LTD.

Calibrating Technician Signature:



ORIFICE METER CALIBRATION

DATE: Jan 9/2020

CONSOLE I.D. MU 1012

	RUN 1	RUN 2	RUN 3
MD= mol. wt. dry air	28.967	28.967	28.967
Pb=bar. pressure "Hg	28.25	28.25	28.25
Y=gas meter factor	0.9915	0.9915	0.9938
Delta H=	0.5	1	1.5
Ri=int. gas meter vol.	0	0	0
Rf=final gas meter vol.	2.05	2.91	3.64
min. samp	5	5	5
Qm=Y(Rf-Ri)/^T(FT3/MIN)	0.406515	0.577053	0.7234864
To=meter outlet Temp (oF)	69	72	75
Tm=meter out temp. (oR)	529	532	535
Pm=Pb + ^H	28.286792	28.3235835	28.3603753
SQRT(Tm/Pm*H/Md)	0.5681581	0.80524856	0.98835912
Ko=orifice const.	0.7154962	0.71661476	0.73200761

Ko MEAN = 0.7213729

Ko*4*144= 415.51077

McCALL ENVIRONMENTAL LTD.

Calibrating Technician Signature:

ORIFICE METER CALIBRATION

DATE: Jan 9/2020

CONSOLE I.D. MU 1012

	RUN 4	RUN 5	RUN 6
MD= mol. wt. dry air	28.967	28.967	28.967
Pb=bar. pressure "Hg	28.25	28.25	28.25
Y=gas meter factor	0.9938	0.9947	0.9947
Delta H=	2	2.5	3
Ri=int. gas meter vol.	0	0	0
Rf=final gas meter vol.	4.22	4.7	5.18
min. samp	5	5	5
Qm=Y(Rf-Ri)/^T(FT3/MIN)	0.8387672	0.935018	1.0305092
To=meter outlet Temp (oF)	78	79	81
Tm=meter out temp. (oR)	538	539	541
Pm=Pb + ^H	28.397167	28.4339588	28.4707506
SQRT(Tm/Pm*H/Md)	1.1437125	1.27906897	1.40283968
Ko=orifice const.	0.7333724	0.73101453	0.734588

Ko MEAN = 0.7329916

Ko*4*144= 422.20319

McCALL ENVIRONMENTAL LTD.


Calibrating Technician Signature:



Analytical Report

Bill To: McCall Environmental 6733 Buchanan Road Coldstream, BC, Canada V1B 3C5	Project ID: CF-12 Project Name: Project Location: Lavington, BC LSD: P.O.:	Lot ID: 1407582 Control Number: Date Received: Feb 12, 2020 Date Reported: Feb 14, 2020 Report Number: 2490761
Attn: Accounts Payable Sampled By: D.Lawrence Company: McCall Env.	Proj. Acct. code:	

	Reference Number	1407582-1	1407582-2	1407582-3	
	Sample Date	Feb 11, 2020	Feb 11, 2020	Feb 11, 2020	
	Sample Time	NA	NA	NA	
	Sample Location				
	Sample Description	Pinnacle Pellet-CF-12 / Test 1	Pinnacle Pellet-CF-12 / Test 2	Pinnacle Pellet-CF-12 / Test 3	
	Matrix	Water	Water	Water	
Analyte	Units	Results	Results	Results	Nominal Detection Limit
Aggregate Organic Constituents					
Oil and Grease	Total	mg/sample	<2	<2	<2
Volume	Sample volume	mL	310	310	320
pH adjustment	required prior to O&G extraction		Yes	Yes	Yes

Approved by: 
 Carol Nam, Dipl. T.
 Quality Officer

Methodology and Notes

Bill To: McCall Environmental 6733 Buchanan Road Coldstream, BC, Canada V1B 3C5	Project ID: CF-12	Lot ID: 1407582
Attn: Accounts Payable	Project Name:	Control Number:
Sampled By: D.Lawrence	Project Location: Lavington, BC	Date Received: Feb 12, 2020
Company: McCall Env.	LSD:	Date Reported: Feb 14, 2020
	P.O.:	Report Number: 2490761
	Proj. Acct. code:	

Method of Analysis

Method Name	Reference	Method	Date Analysis Started	Location
Oil and Grease in water (VAN)	BCELM	* Oil & Grease in Water - Direct Hexane Extraction, Oil & Grease <i>* Reference Method Modified</i>	Feb 13, 2020	Element Vancouver

References

BCELM	B.C. Environmental Laboratory Manual
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Please direct any inquiries regarding this report to our Client Services group.

Results relate only to samples as submitted.

The test report shall not be reproduced except in full, without the written approval of the laboratory.


- i. Average hourly dryer exit gas temperature during testing;
43.2 °C
- ii. Average hourly dryer ODT for the biomass dryer system for the previous month;
28.1 ODT/hr
- iii. 90th percentile hourly ODT throughput for the biomass dryers (Section 4.3);
36.1 ODT/hr
- iv. Average hourly throughput ODT for the biomass dryer system during stack testing;
31.0 ODT/hr



This is to verify that
Matthew McCall
has successfully completed
a course of study in
Source Testing for Particulates
(35 hours)

Endorsed by
The B.C. Ministry of Environment

Dated at Burnaby, British Columbia, Canada
December 14, 1990


DEAN


REGISTRAR

BRITISH COLUMBIA INSTITUTE OF TECHNOLOGY



North Carolina State University Environmental Programs

This certificate awarded to

Danny Lawrence

for satisfactory completion of course and examination for

SI: 414 Quality Assurance for Source Emission Measurements

Irma F. Vanderhall
Manager

Christine S. Murphy
Registrar

May 22, 2000

Date Completed

3.5 CEUs

Awarded under EPA Assistance Agreement CT - 825724

